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Realistic FDTD GPR antenna models optimised using a novel linear/non-linear Full Waveform Inversion

Iraklis Giannakis, Antonios Giannopoulos, and Craig Warren

Abstract—Finite-Difference Time-Domain (FDTD) modelling of Ground Penetrating Radar (GPR) is becoming regularly used in model-based interpretation methods like full waveform inversion (FWI), and machine learning schemes using synthetic training data. Oversimplifications in such forward models can compromise the accuracy and realism with which real GPR responses can be simulated, and this degrades the overall performance of the aforementioned interpretation techniques. Therefore, a forward model must be able to accurately simulate every part of the GPR problem that can affect the resulting scattered field. A key element is the antenna system and excitation waveform, so the model must contain a complete description of the antenna including the excitation source and waveform, the geometry, and the dielectric properties of materials in the antenna. The challenge is that some of these parameters are not known or easily measured, especially for commercial GPR antennas that are used in practice. We present a novel hybrid linear/non-linear FWI approach which can be used, with only knowledge of the basic antenna geometry, to simultaneously optimise the dielectric properties and excitation waveform of the antenna, and minimise the error between real and synthetic data. The accuracy and stability of our proposed methodology is demonstrated by successfully modelling a Geophysical Survey Systems (GSSI) Inc. 1.5 GHz commercial antenna. Our framework allows accurate models of GPR antennas to be developed without requiring detailed knowledge of every component in the antenna. This is significant because it allows commercial GPR antennas, regularly used in GPR surveys, to be more readily simulated.

Keywords—Antennas, commercial, FDTD, FWI, GPR, hybrid optimisation, linear inversion, non-linear inversion.

I. INTRODUCTION

Ground Penetrating Radar (GPR) has been successfully applied to sensing problems across a wide spectrum of scales – from landmine detection at very shallow depths, to mapping the thickness of glaciers [1]. Consequently, different antennas have been proposed in order to address the unique requirements of each GPR sensing problem – dipoles [2], bowties [3], horns [4], spirals [5], and more complicated non-conventional antennas [6] specifically designed for GPR applications using different sizes, excitation pulses, and absorbing materials [1]. Despite the diversity of real GPR antennas, numerical models

often include basic excitation models and simplified antenna structures [7], [8], [9] which can lead to generic and non-exact outputs when these models are used to compare real to predicted GPR data.

The antenna system is a dominant part of the simulation and should be accurately modelled if the simulation is to replicate the behaviour of a given GPR system [10], [11]. The directivity pattern, ringing noise, shape of the waveform, and the coupling between the antenna and the ground are directly related to the antenna system [10], [12]. Models using simplified excitation sources, such as Hertzian dipoles, especially for high frequency applications, can produce significantly different responses from real measurements [10]. Therefore, these models cannot be easily employed either as a forward solver for inversion purposes, or for generating synthetic training sets for machine learning applications [13].

Numerical solvers, and in particular the finite-difference time-domain (FDTD) method [14], have been extensively applied to model antennas, primarily for design purposes [15]. Many researchers have created numerical models of their bespoke GPR systems in an effort to study and investigate performance. In [16], a bowtie GPR antenna is modelled using FDTD and its resistive loading is designed to minimise the voltage reflection. The authors of [16] were the first to consider the problems arising from modelling GPR antennas using FDTD, due to discretisation (staircasing) errors, and most importantly due to simplified feeding mechanisms. This problem is tackled in [17], [18], [2] by using a 1D-FDTD model embedded in a 3D numerical solver to try to simulate a coaxial cable as a feeding mechanism. [17], [18], [2] can be considered the first to attempt numerical modelling of a GPR scenario using a custom made bowtie antenna placed on top of oil emulsions. The latter are frequently used to replicate the dielectric behaviour of soils for lab scale experiments [19], [20], and for validating GPR antenna models [10]. An accurate implementation of an antenna system in a numerical solver like FDTD can become computationally costly. To tackle this, a hybrid numerical scheme is described in [21] that uses the Method of Moments (MoM) and FDTD for modelling a dipole antenna and the soil respectively. This work is a continuation of [22] in which equivalent point sources are used to approximate the effects of the antenna structure without modelling its geometry. Approximating the antenna using linear functions became a very attractive and popular technique for modelling off-ground antennas. The equivalent sources are calibrated using real measurements [4], [23], avoiding costly numerical

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simulations and the need for accurate knowledge of the antenna geometry, dielectric properties etc... The main drawbacks of this approach are that it requires knowledge of the system excitation, and it assumes that the scattering sources are placed in the far-field region of the antenna [4]. Hence, equivalent sources were successfully applied primarily for modelling custom made off-ground horn antennas [4], [23], [24]. In [25], an equivalent sources scheme is suggested which models the global reflection and transmission coefficients in an effort to model the near-field behaviour of a custom made Vivaldi antenna. The near-field formulation has been successfully tested in layered media, but further validation is needed in more realistic scenarios.

As computational resources have increased in power and accessibility, numerical modelling of antennas using FDTD gained in popularity [26]–[33]. Nonetheless, commercial antennas, which are available to the end-user, remained a black box and only a few researchers have tried to tackle this issue by fully simulating a commercial GPR system [10], [34], [35]. In [10] and [34], a 1.5 GHz commercial antenna from Geophysical Survey Systems (GSSI) Inc. is modelled using FDTD. A fine 1 mm grid is employed in an effort to minimise numerical dispersion [15] and avoid staircasing effects. Furthermore, a Taguchi optimisation is used in order to fine-tune the dielectric properties of the antenna. The cost function of the optimisation is the difference between the real and the synthetic free-space response. A Gaussian voltage source is used as an excitation, and the central frequency is decided from the Taguchi optimisation. This limits the accuracy of the resulting antenna model since it constrains the pulse to be Gaussian-shaped. Using global optimisers to derive the optimised pulse without any given constraints will vastly increase the optimisation parameters which will, in turn, increase the required computational resources to an unreasonable level.

In this paper, in order to address this issue, instead of a Taguchi optimisation, a hybrid linear/non-linear least squares scheme that simultaneously updates the dielectric properties and the corresponding optimised pulse is introduced. We use a non-linear least squares optimisation to fine-tune the dielectric properties of a given antenna and simultaneously the optimised pulse is expressed linearly with respect to these properties. Thus, the shape of the pulse is not bounded by any constraints, and the computational requirements of the optimisation are not increased.

A similar hybrid linear/non-linear optimisation is proposed in [36] to evaluate the optimised wavenumbers for solving the 2.5-D Helmholtz equation for electrical resistivity tomography. A modified version of [36] using particle swarm optimisation is suggested in [37] in order to approximate Havriliak-Negami functions with multi-Debye expansions. The simultaneous evaluation of the medium parameters and of the effective wavelet in seismic FWI has been a subject of investigation since the early 1980's [38], [39]. For GPR, wavelet estimation as part of FWI has been successfully applied by different authors mostly for cross-borehole applications. In particular, a hybrid least-squares/simplex-search FWI is employed in [40], assuming a homogeneous half space and using a single dipole

to describe the antenna system. In [41] and [42] a FWI scheme is proposed in which the pulse is part of the unknowns and the applicability of multiple wavelets is examined to address the fact that the effective wavelet is affected by the location of the transmitter. This results from describing the antenna with a single point source without incorporating its physical structure in the numerical model. A similar approach is used by [43] to tackle the challenging problem of estimating the radius of a rebar inside concrete. In [44], a hybrid least-squares/cascaded algorithm is used in order to approximate a Wu-King type antenna by equivalent sources. The resulting antenna approximates the far field behaviour of the actual antenna with sufficient accuracy. Similar to all the approaches that employ equivalent sources, the modelled antenna in [44] does not contain any information regarding the near-field interactions of the antenna structure with the background, thus it is not recommended for modelling ground-coupled antennas especially for high frequency near-field problems. Lastly, effective wavelet estimation of point sources prior to FWI is also applied by [45] for cross-borehole tomography, and [46] for estimating the chloride content of concrete.

Apart from [36], all the papers mentioned above that use gradient-based optimisation approaches, do not include the linear part of the inversion in the evaluation of the partial derivatives. In other words, the gradients are calculated given that the output of the linear part, the effective wavelet, is constant in each step and is not affected by the variation of the non-linear parameters related to the medium properties. In this paper we follow the approach in [36], but instead of using a central-difference method we evaluate the Jacobian analytically. As far as we are aware, such an analytical evaluation of the true Jacobian in hybrid linear/non-linear optimisation problems has not been attempted before.

To avoid instabilities in the linear step of the optimisation, in contrast to [40] and [44], a Levenberg-Marquardt damped least squares method [47], also known as Tikhonov regularization method [48], [49]) is used, and all the calculations take place directly in time domain. A similar regularisation method is applied in the frequency domain in [46] to evaluate an effective wavelet prior to FWI. Nonetheless, the regularisation parameter in [46] is chosen in an arbitrary manner and the authors do not address the sensitivity of the deconvolved pulse to the regularisation parameter. Here, the regularisation parameter is chosen based on the L-curve method [50], [51] which balances accuracy and stability.

The proposed hybrid FWI scheme is tested by modelling a GSSI 1.5 GHz commercial antenna [10]. The resulting model is a finely-discretised representation of the GSSI 1.5 GHz antenna implemented in a complete numerical solver like FDTD using an optimised and unconstrained excitation pulse. The current model is not restricted only to far-field applications and can accurately simulate the near-field behaviour of the GSSI 1.5 GHz antenna including ringing noise, coupling effects, directivity etc... The proposed methodology can be applied in a straightforward manner to other non-custom antenna systems for which knowledge about the excitation pulse and the dielectric properties are often unknown due to confidentiality issues. In addition, the analytical evaluation of

the Jacobian matrix for hybrid linear/non-linear inversion and the L-curve approach can be extrapolated in a similar manner for traditional GPR and seismic FWI for which the effective wavelet is part of the unknown parameters.

II. HYBRID LINEAR/NON-LINEAR INVERSION

The proposed inversion scheme is intended to be applied to antennas with unknown dielectric properties and excitation sources. This is a common occurrence when modelling commercial antennas for which these properties are unknown for confidentiality reasons. Nonetheless, the geometrical properties of the antenna can usually be obtained by inspection. Thus, in the proposed hybrid FWI it is assumed that the geometry of the antenna is known and accurately modelled in the FDTD numerical simulator.

Another assumption of the proposed FWI is linearity, which is valid for the majority of electromagnetic (EM) problems [15] when low amplitude fields are used. The linear step of the optimisation is a constrained deconvolution. Consequently, non-linear EM phenomena are assumed to be negligible, and dielectric properties are not related to the amplitude of the field. In addition, the FDTD forward solver used in this paper implements linear isotropic media. Using a forward solver that incorporates non-linear media would greatly increase the complexity and computational resources of every aspect of the FWI.

The modelled antenna is not necessarily an exact replica of the real antenna. It is an apparent antenna that is intended to accurately replicate the behaviour and performance of the real antenna.

A. Linear Least-Squares Inversion

The explicit representation of the received electric field due to a distribution of current densities is given by [52]

$$\mathbf{E}^s = \int_V \int_0^\tau \mathbf{G}(\mathbf{x}, \mathbf{x}', t, t') \mathbf{J}(\mathbf{x}', t') dt' dV(\mathbf{x}') \quad (1)$$

where, $\mathbf{G} = [G_x, G_y, G_z]$ is the Green's function that acts on the current density vector $\mathbf{J} = [J_x, J_y, J_z]$, $\mathbf{E}^s = [E_x, E_y, E_z]$ is the electric field, $\mathbf{x}' = [x, y, z]$ are the Cartesian coordinates of the transmitter, \mathbf{x} are the Cartesian coordinates of the receiver, τ is time, and V is the investigated 3D volume.

For simplicity it is assumed that the transmitter and the receiver are at known positions and that the transmitter-receiver separation stays constant. This is a standard configuration for common-offset antennas most frequently employed in GPR applications [1]. In addition, the components of the excitation source and the received field are usually known and they are placed for convenience to be parallel to one of the Cartesian axes. Lastly, the unknown parts of the model are the dielectric properties of the antenna, thus, the Green's function can be expressed with respect to the dielectric properties of the antenna assuming the rest of the model (i.e. chosen background) is constant throughout the FWI. Based on the above, equation (1) can be restated as

$$E_i^s = \int_0^\tau G_{i,j}(\mathbf{p}, t, t') I_j(t') dt' \quad (2)$$

where $\mathbf{p} = [p_1, p_2, p_3, \dots, p_n]$ is a vector that contains the dielectric properties of the antenna parts, assuming that the geometry is known, I_j is the induced current, $j \in \{x, y, z\}$ is the component of the transmitted field, and $i \in \{x, y, z\}$ is the component of the received field. For co-polarised antennas $i = j$.

Equation (2) is a convolution and can be re-written as

$$E_i^s(\mathbf{p}, t) = G_{i,j}(\mathbf{p}, t) * I_j(t) \quad (3)$$

$$G_{i,j}(\mathbf{p}, t) = G_{m,i,j}(\mathbf{p}, t) * G_{r,i,j}(t) \quad (4)$$

$$I_j(t) = P_j(t) * C_j(t) \quad (5)$$

where $G_{i,j}$ is expressed as the Green's function of the model $G_{m,i,j}$ convolved with the Green's function of the receiver $G_{r,i,j}$. Notice that FDTD can model $G_{m,i,j}$ using a delta function to excite the FDTD solver with sufficient accuracy for a specified frequency range. Nonetheless, electronic components in the antenna and post-processing associated with $G_{r,i,j}$ cannot be modelled using FDTD without prior knowledge. A similar division occurs in (5) in which the excitation source is expressed as a convolution between the initial applied pulse P_j (Gaussian, delta function and so on) with the correction C_j . As it is stated earlier, the above formulation is not valid when non-linear electromagnetic phenomena are present.

Due to the interchangeable nature of convolution, equation (3) can be written as

$$E_i^s(\mathbf{p}, t) = E_i^c(\mathbf{p}, t) * R_{i,j}(t) \quad (6)$$

$$E_i^c(\mathbf{p}, t) = G_{m,i,j}(\mathbf{p}, t) * P_j(t) \quad (7)$$

$$R_{i,j}(t) = C_j(t) * G_{r,i,j}(t) \quad (8)$$

Notice that $E_i^c(\mathbf{p}, t)$ can be evaluated for a given vector \mathbf{p} using FDTD excited by $P_j(t)$. The term $R_{i,j}(t)$ expresses the unknown receiver effects plus the correction that is convolved with the initial excitation source. The convolution in (6) can be numerically evaluated as follows

$$\mathbf{Q} = \mathbf{K}\mathbf{X} \quad (9)$$

$$\mathbf{K} = \begin{bmatrix} E_i^c(\mathbf{p}, t_1) & 0 & \dots & 0 \\ E_i^c(\mathbf{p}, t_2) & E_i^c(\mathbf{p}, t_1) & \dots & 0 \\ E_i^c(\mathbf{p}, t_3) & E_i^c(\mathbf{p}, t_2) & \dots & 0 \\ E_i^c(\mathbf{p}, t_4) & E_i^c(\mathbf{p}, t_3) & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ E_i^c(\mathbf{p}, t_N) & E_i^c(\mathbf{p}, t_{N-1}) & \dots & E_i^c(\mathbf{p}, t_1) \end{bmatrix}$$

$$\mathbf{Q} = [E_i^s(\mathbf{p}, t_1), E_i^s(\mathbf{p}, t_2), E_i^s(\mathbf{p}, t_3) \dots E_i^s(\mathbf{p}, t_N)]^T \quad (10)$$

$$\mathbf{X} = [R_{i,j}(t_1), R_{i,j}(t_2), R_{i,j}(t_3) \dots R_{i,j}(t_N)]^T \quad (11)$$

where N is the number of FDTD iterations, T corresponds to the transpose sign, \mathbf{Q} is a vector containing the received signal, \mathbf{K} is a matrix which is calculated using FDTD, and \mathbf{X} is the unknown correction term which includes features

that cannot be implemented in FDTD either due to a lack of information or due to limitations of FDTD (e.g. modelling electronic components in the GPR transducer).

The idea behind the proposed method is to use a series of controlled experiments (e.g. direct coupling in free space) in order to fine tune an antenna model with a given geometry. The controlled measurements represent the \mathbf{Q} vector, the measurements taken using the real antenna with the actual excitation pulse and the actual receiver effects. With a given geometry and a set of dielectric properties \mathbf{p} , the matrix \mathbf{K} can be calculated using FDTD. Subsequently the vector \mathbf{X} is derived by solving the linear system of equations in (9).

Notice that when only one controlled experiment is used, the system of equations in (9) becomes well-determined and an exact fit will occur regardless of \mathbf{K} , given $\det(\mathbf{K}) \neq 0$. Thus, approaches using only one controlled experiment [53] to calibrate the modelled antenna lead to non-uniqueness as the fitted function has higher dimensions compared to the data, similar to fitting the best line to a point. Hence, the resulting antenna is not reliable for universal applications despite the fact that the fit is good for the specific single controlled experiment. In addition, similar calibration approaches applied to either frequency or time domain need a regularisation parameter in order to overcome the instabilities arising from dividing by zero in frequency domain. This becomes clear when (6) is solved in the frequency domain $\hat{R}_{i,j}(\omega) = \hat{E}_i^s(\mathbf{p}, \omega) / \hat{E}_i^c(\mathbf{p}, \omega)$. Frequencies where $\hat{E}_i^c(\mathbf{p}, \omega)$ become close to zero are susceptible to noise and create instabilities that reduces the overall reliability of the resulting $\hat{R}_{i,j}$.

By using more than one controlled experiment the system of (9) becomes over-determined

$$\begin{bmatrix} \mathbf{Q}_1 \\ \mathbf{Q}_2 \\ \vdots \\ \mathbf{Q}_M \end{bmatrix} = \begin{bmatrix} \mathbf{K}_1 \\ \mathbf{K}_2 \\ \vdots \\ \mathbf{K}_M \end{bmatrix} \mathbf{X} \quad (12)$$

where M is the number of controlled experiments. For convenience the following matrices are introduced

$$\mathbf{Y} = [\mathbf{Q}_1, \mathbf{Q}_2, \dots, \mathbf{Q}_M]^T \quad (13)$$

$$\mathbf{A} = [\mathbf{K}_1, \mathbf{K}_2, \dots, \mathbf{K}_M]^T. \quad (14)$$

The over-determined system can be solved using the Tikhonov regularised least-squares method

$$\mathbf{X} = (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \mathbf{A}^T \mathbf{Y} \quad (15)$$

where λ is the regularisation parameter, and \mathbf{I} is the identity matrix. The regularisation factor λ is added to suppress the resulting \mathbf{X} vector and prevent its norm from reaching extreme values due to high signal-to-noise ratio at frequencies with amplitudes close to zero.

The \mathbf{X} vector resulting from (15) minimises the following function $\min_{\mathbf{X} \in \mathbb{R}^N} \|\mathbf{A}\mathbf{X} - \mathbf{Y}\|_2^2 + \lambda^2 \|\mathbf{X}\|_2^2$ given a regularisation

parameter λ and a vector \mathbf{p} , necessary to calculate \mathbf{A} . The vector \mathbf{p} , and its corresponding optimised \mathbf{X} , that minimises the difference between the real and the synthetic measurements, is derived through the following non-linear optimisation.

B. Non-Linear Inversion

The dielectric properties of the antenna are assumed to be isotropic, linear, and dispersion-less. In other words, the dielectric properties of the different parts of the antenna are approximated with a constant permittivity and conductivity $p_b = [\epsilon_b, \sigma_b]$.

Substituting (15) to (12) results in

$$\mathbf{Y} = \mathbf{A} (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \mathbf{A}^T \mathbf{Y}. \quad (16)$$

The only variables to be optimised in (16) are the dielectric properties of the antenna. The latter are given in vector form $\mathbf{p} = [p_1, p_2, \dots, p_n]$, where n is the number of the antenna parts. The vector \mathbf{X} is now described algebraically as a function of \mathbf{A} , i.e. as a function of the dielectric properties of the antenna. Thus, the dimensionality of the optimisation space is greatly reduced.

It is apparent that equation (16) is valid only when

$$\mathbf{I} = \mathbf{A} (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \mathbf{A}^T, \quad (17)$$

which holds true regardless of \mathbf{p} , if the system of equations (9) is well-determined using only one controlled experiment, for $\lambda = 0$, and when $\det(\mathbf{A}) \neq 0$.

When more than one controlled experiment is used, a non-linear least squares inversion is employed that minimises the following function

$$\min_{\mathbf{p} \in \mathbb{R}^n} \|\mathbf{A} (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \mathbf{A}^T \mathbf{Y} - \mathbf{Y}\|_2^2. \quad (18)$$

Introducing the vector \mathbf{D}

$$\mathbf{D} = \mathbf{A} (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \mathbf{A}^T \mathbf{Y}, \quad (19)$$

equation (18) can be simplified as

$$\min_{\mathbf{p} \in \mathbb{R}^n} \|\mathbf{D} - \mathbf{Y}\|_2^2. \quad (20)$$

Non-linear least squares inversion is an iterative method that linearises the problem in each iteration. An initial set of dielectric properties \mathbf{p} is chosen which is used to evaluate the vector \mathbf{D}_p . Subsequently, the vector \mathbf{Y} is approximated by a first-order Taylor series expansion

$$\mathbf{Y} = \mathbf{D}_{p_w} + \mathbf{J}_{p_w} \Delta \mathbf{p}_w \quad (21)$$

where the subscript w represents the number of the iteration. The Jacobian matrix \mathbf{J} has $M \cdot N \times n$ dimensions (M number of controlled experiments, N number of time iterations in each experiment, and n is the length of the vector \mathbf{p}) and

contains the partial derivatives of the vector \mathbf{D} with respect to the dielectric properties \mathbf{p} .

$$\mathbf{J} = \begin{bmatrix} \frac{\partial D_1}{\partial p_1} & \frac{\partial D_1}{\partial p_2} & \frac{\partial D_1}{\partial p_3} & \cdots & \frac{\partial D_1}{\partial p_n} \\ \frac{\partial D_2}{\partial p_1} & \frac{\partial D_2}{\partial p_2} & \frac{\partial D_2}{\partial p_3} & \cdots & \frac{\partial D_2}{\partial p_n} \\ \frac{\partial D_3}{\partial p_1} & \frac{\partial D_3}{\partial p_2} & \frac{\partial D_3}{\partial p_3} & \cdots & \frac{\partial D_3}{\partial p_n} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \frac{\partial D_{M \cdot N}}{\partial p_1} & \frac{\partial D_{M \cdot N}}{\partial p_2} & \frac{\partial D_{M \cdot N}}{\partial p_3} & \cdots & \frac{\partial D_{M \cdot N}}{\partial p_n} \end{bmatrix}$$

Where $\frac{\partial D_k}{\partial p_g}$ is a vector containing the partial derivatives with respect to permittivity and conductivity

$$\frac{\partial D_k}{\partial p_g} = \left[\frac{\partial D_k}{\partial \epsilon_g}, \frac{\partial D_k}{\partial \sigma_g} \right]. \quad (20)$$

Using least squares the vector $\Delta \mathbf{p}_w$ in (21) is derived

$$\Delta \mathbf{p}_w = \left(\mathbf{J}_{\mathbf{p}_w}^T \mathbf{J}_{\mathbf{p}_w} \right)^{-1} \mathbf{J}_{\mathbf{p}_w}^T (\mathbf{Y} - \mathbf{D}_{\mathbf{p}_w}). \quad (21)$$

Subsequently the vector \mathbf{p} is updated

$$\mathbf{p}_{w+1} = \mathbf{p}_w + \Delta \mathbf{p}_w \quad (22)$$

and the procedure is repeated until (18) converges to a minimum. Given an optimised set of dielectric properties \mathbf{p} , the correction term \mathbf{X} can be calculated in a straightforward manner using (15).

The hybrid linear/non-linear FWI evaluates permittivity and conductivity simultaneously in contrast to [54] in which a permittivity distribution is initially derived and subsequently the optimised conductivity profile is derived based on the pre-estimated permittivity distribution. This is due to the fact that [54] uses a gradient-based cascaded scheme in which the incremental step is defined by the user. This results in a bias towards permittivity changes since the sensitivity of conductivity is orders of magnitude less than the sensitivity of permittivity. A solution to this is given in [52] in which the incremental steps are adjusted accordingly in order to regulate the sensitivity discrepancies. The proposed FWI overcomes the aforementioned issues since the incremental step is calculated directly in (21). In the case study presented here, the proposed algorithm is proven to be stable and robust despite the sensitivity gap between permittivity and conductivity. In the presence of ill-conditioned Jacobians due to low sensitivity at parts of the antenna, inadequate controlled experiments etc., it is advised to use a Marquardt non-linear least squares [47].

Non-linear inversion is a convex optimisation and assumes that the initial model is relatively close to the real one. Convex optimisers are frequently employed in FWI for both GPR and seismic methods, and the importance of the initial model has been stressed by many authors [54], [55], [56]. The current method is proven to be not as sensitive to the initial conditions as a generic FWI. This is probably due to the fact that the geometry of the antenna is constrained and the unknown parameters are orders of magnitude smaller compared to 3D tomography. Nonetheless, it is preferable to choose a rational set for the initial vector \mathbf{p} to ensure fast convergence and stability.

C. L-curve and selection of λ

Regularisation is an essential element in deconvolution in order to repress extreme solutions arising either from noise or from frequencies with amplitudes close to zero [1]. It is apparent that the final output of the deconvolution is sensitive to λ selection and a systematic way of choosing an appropriate λ should be applied. Prior methods that neglect regularisation or chose it in an arbitrary manner result in unreliable outputs due to the non-uniqueness of the problem.

The well-known L-curve [50], [51] method is chosen in this paper in an effort to balance stability and accuracy. During the linear step of the FWI the following function is minimised $\min_{\mathbf{X} \in \mathbb{R}^N} \|\mathbf{A}\mathbf{X} - \mathbf{Y}\|_2^2 + \lambda^2 \|\mathbf{X}\|_2^2$ given a vector \mathbf{p} , evaluated in the non-linear step, and λ as defined by the user. The L-curve tries to balance the two parameters of the minimisation i.e. $\eta_\lambda = \|\mathbf{A}\mathbf{X} - \mathbf{Y}\|_2^2$ and $\rho_\lambda = \|\mathbf{X}\|_2^2$. Large values of λ will repress ρ_λ while compromise η_λ . On the other hand, for $\lambda = 0$ the problem transforms to naive least-squares with small η_λ and unstable (large) ρ_λ .

Plotting $(\eta_\lambda, \rho_\lambda)$ results in an exponentially decaying function. A log-log plot of this function results in a curve that looks like the letter 'L', hence the name L-curve method. The λ value that corresponds to the critical point where ρ_λ starts to converge to a minimum is the point where $\min_{\lambda \in \mathbb{R}} \|\mathbf{A}\mathbf{X} - \mathbf{Y}\|_2^2 + \|\mathbf{X}\|_2^2$ given a vector \mathbf{p} , and the controlled experiments \mathbf{Y} . Here, a brute force approach is followed in which the hybrid linear/non-linear FWI is executed with different λ . Subsequently the L-curve is plotted and the appropriate λ associated with the critical point of the curve is chosen.

D. Jacobian calculation

The Jacobian matrix can be expressed in a more compact form as follows

$$\mathbf{J} = \begin{bmatrix} \frac{\partial \mathbf{D}}{\partial p_1} & \frac{\partial \mathbf{D}}{\partial p_2} & \cdots & \frac{\partial \mathbf{D}}{\partial p_n} \end{bmatrix} \quad (23)$$

where

$$\frac{\partial \mathbf{D}}{\partial p_g} = \left[\frac{\partial D_1}{\partial p_g} \quad \frac{\partial D_2}{\partial p_g} \quad \cdots \quad \frac{\partial D_{M \cdot N}}{\partial p_g} \right]^T. \quad (24)$$

The simplest way to calculate the derivative is through a central finite-difference approximation (first order approximations can be applied in a similar manner)

$$\frac{\partial \mathbf{D}(p_g)}{\partial p_g} \approx \frac{\mathbf{D}(p_g + \Delta p_g) - \mathbf{D}(p_g - \Delta p_g)}{2\Delta p_g}. \quad (25)$$

From (19) and (24) it follows that the analytical expression of the Jacobian is

$$\frac{\partial \mathbf{D}}{\partial p_g} = \frac{\partial \left(\mathbf{A} \left(\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I} \right)^{-1} \mathbf{A}^T \right)}{\partial p_g} \mathbf{Y}. \quad (26)$$

$$\frac{\partial \mathbf{D}}{\partial p_g} = \left(\frac{\partial \mathbf{A}}{\partial p_g} (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \mathbf{A}^T + \mathbf{A} \left(-(\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \left(\left(\frac{\partial \mathbf{A}}{\partial p_g} \right)^T \mathbf{A} + \mathbf{A}^T \frac{\partial \mathbf{A}}{\partial p_g} \right) (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \right) \mathbf{A}^T + \mathbf{A} (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \frac{\partial \mathbf{A}^T}{\partial p_g} \right) \mathbf{Y} \quad (30)$$

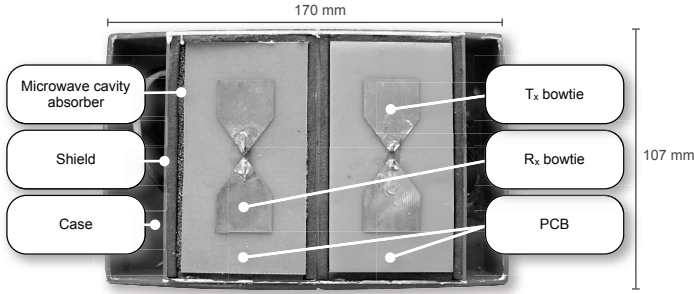


Fig. 1. The GSSI 1.5 GHz antenna photographed from above with the plastic skid removed [10]

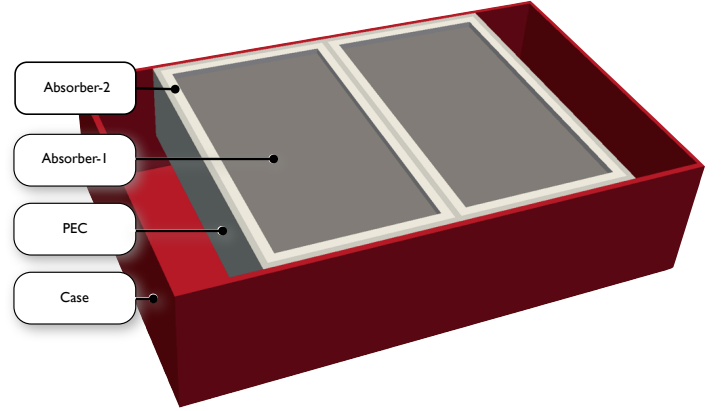


Fig. 2. The modelled GSSI 1.5 GHz antenna without the plastic skid, the PCB, and the Tx-Rx bowties [10]

$$\begin{aligned} \frac{\partial \mathbf{D}}{\partial p_g} &= \frac{\partial \mathbf{A}}{\partial p_g} (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \mathbf{A}^T \mathbf{Y} + \\ &+ \mathbf{A} \frac{\partial (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1}}{\partial p_g} \mathbf{A}^T \mathbf{Y} + \\ &+ \mathbf{A} (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \frac{\partial \mathbf{A}^T}{\partial p_g} \mathbf{Y}. \end{aligned} \quad (27)$$

Furthermore, the derivative of the second term in (27) is equal to [57]

$$\begin{aligned} \frac{\partial (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1}}{\partial p_g} &= \\ -(\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \frac{\partial (\mathbf{A}^T \mathbf{A})}{\partial p_g} (\mathbf{A}^T \mathbf{A} + \lambda^2 \mathbf{I})^{-1} \end{aligned} \quad (28)$$

where

$$\frac{\partial (\mathbf{A}^T \mathbf{A})}{\partial p_g} = \left(\frac{\partial \mathbf{A}}{\partial p_g} \right)^T \mathbf{A} + \mathbf{A}^T \frac{\partial \mathbf{A}}{\partial p_g}. \quad (29)$$

Substituting (29) to (28) and subsequently substituting (28) to (27) results in (30). As explained earlier, the matrix \mathbf{A} can be calculated directly using FDTD. Thus, the only unknown in (30) is the matrix $\frac{\partial \mathbf{A}}{\partial p_g}$ which can be evaluated by calculating the following derivative $\frac{\partial \mathbf{E}_p}{\partial p_g}$ (9). The latter is the sensitivity of Maxwell's equations to a variation of the dielectric properties in a defined volume. The sensitivity of Maxwell's equations with respect to ϵ and σ is discussed in [52], [58]. A convenient and accessible proof can be derived by evaluating the derivative of Maxwell's equations directly. Following this approach, the sensitivity with respect to permittivity is given by

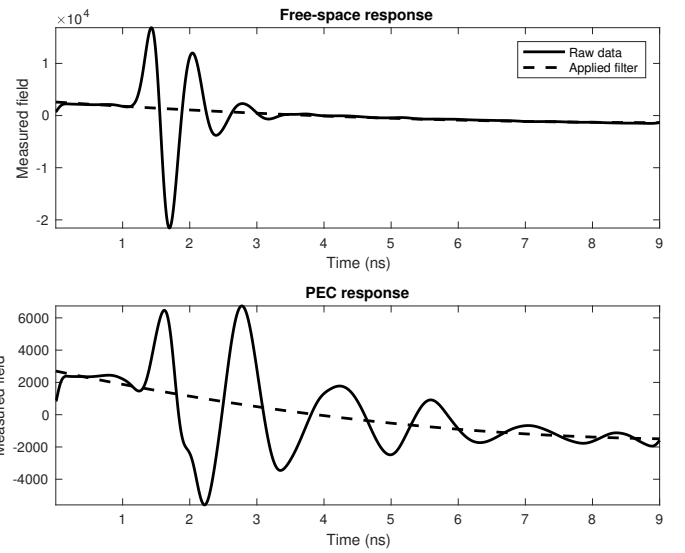


Fig. 3. Raw data from the free-space and the PEC responses (solid lines). Dotted lines represent the static current phenomena approximated with a second order polynomial. The latter are filtered out.

$$\begin{aligned} \nabla \times \frac{\partial \mathbf{H}}{\partial \epsilon_r} &= \epsilon \frac{\partial}{\partial t} \frac{\partial \mathbf{E}}{\partial \epsilon_r} + \sigma \frac{\partial \mathbf{E}}{\partial \epsilon_r} \\ &+ \int_V \delta(\mathbf{r} - \mathbf{r}') \frac{\partial \mathbf{E}}{\partial t} dV \end{aligned} \quad (31)$$

$$\nabla \times \frac{\partial \mathbf{E}}{\partial \epsilon_r} = \mu \frac{\partial}{\partial t} \frac{\partial \mathbf{H}}{\partial \epsilon_r} + \sigma_\mu \frac{\partial \mathbf{H}}{\partial \epsilon_r}. \quad (32)$$

Where δ is the delta function, $\mathbf{r}' = [i, j, z] \in \{x, y, z\}$ are the coordinates for which the sensitivity is measured,

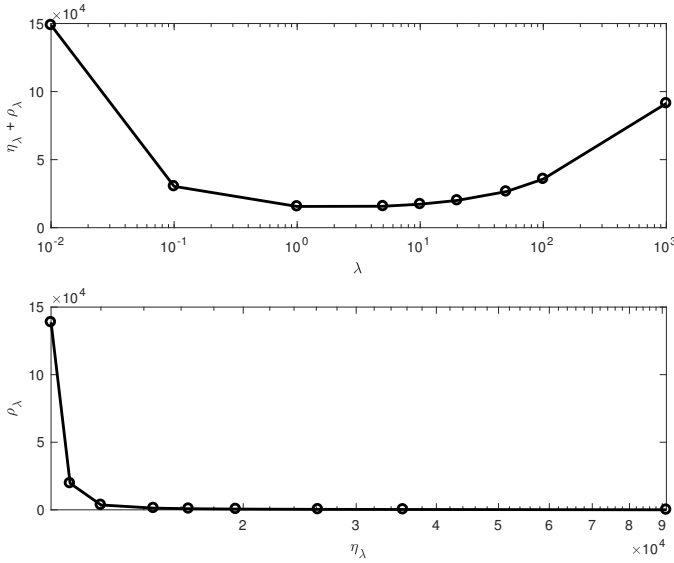


Fig. 4. $(\eta_\lambda, \rho_\lambda)$ and $(\eta_\lambda + \rho_\lambda, \lambda)$ using different λ . For $\lambda = 1$ the solution balances accuracy and stability.

$\mathbf{r} = [x, y, z]$, μ is the magnetic permeability, σ_μ is a term describing the magnetic losses [15], ϵ is the 3D distribution of electric permittivity, σ is the 3D distribution of electric conductivity, \mathbf{H} is the magnetic field, and \mathbf{E} is the electric field. Similarly to (31) and (32), the sensitivity with respect to the conductivity is described by

$$\begin{aligned} \nabla \times \frac{\partial \mathbf{H}}{\partial \sigma_{\mathbf{r}'}}} &= \epsilon \frac{\partial}{\partial t} \frac{\partial \mathbf{E}}{\partial \sigma_{\mathbf{r}'}}} + \sigma \frac{\partial \mathbf{E}}{\partial \sigma_{\mathbf{r}'}}} + \\ &\quad + \int_V \delta(\mathbf{r}' - \mathbf{r}) \mathbf{E} dV \\ \nabla \times \frac{\partial \mathbf{E}}{\partial \sigma_{\mathbf{r}'}}} &= \mu \frac{\partial}{\partial t} \frac{\partial \mathbf{H}}{\partial \sigma_{\mathbf{r}'}}} + \sigma_\mu \frac{\partial \mathbf{H}}{\partial \sigma_{\mathbf{r}'}}}. \end{aligned} \quad (33)$$

Notice that (31)-(33) have the same form as Maxwell's equations but instead of $[\mathbf{E}, \mathbf{H}, \mathbf{J}]$, the following parameters are used for evaluating the derivative with respect to permittivity $\left[\frac{\partial \mathbf{E}}{\partial \epsilon_{\mathbf{r}'}}}, \frac{\partial \mathbf{H}}{\partial \epsilon_{\mathbf{r}'}}}, \int_V \delta(\mathbf{r}' - \mathbf{r}) \frac{\partial \mathbf{E}}{\partial t} dV \right]$ and similarly for the derivative with respect to conductivity $\left[\frac{\partial \mathbf{E}}{\partial \sigma_{\mathbf{r}'}}}, \frac{\partial \mathbf{H}}{\partial \sigma_{\mathbf{r}'}}}, \int_V \delta(\mathbf{r}' - \mathbf{r}) \mathbf{E} dV \right]$. Thus, the sensitivity can be evaluated in a straightforward manner by exciting an FDTD solver with the current density sources described above.

III. CASE STUDY: MODELLING THE GSSI 1.5 GHz ANTENNA

The proposed hybrid linear/non-linear FWI is applied to numerically describe the GSSI 1.5 GHz commercial antenna (Fig. 1). The dielectric properties and effective wavelet of the antenna are fine-tuned based on controlled measurements. In particular, two easily accessible scenarios are investigated, a) the free-space response, and b) the response from a metal plate. The latter describes the scenario in which the antenna is placed right on top of a perfect electric conductor (PEC). The

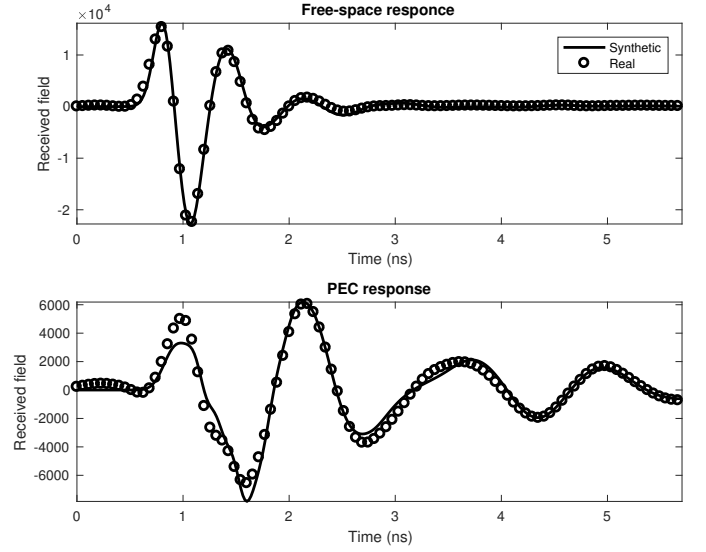


Fig. 5. Real and synthetic A-scans for the two controlled experiments.

forementioned scenarios are chosen primarily based on the fact that it is very easy to reproduce them numerically. In addition, coupling the antenna with a PEC will result in repetitive reflections between the shielding of the antenna and the PEC. This will increase the sensitivity of the measured signal to the dielectric properties of the antenna. It is apparent that further controlled experiments will contribute to a more robust output. Nonetheless, a balance between efficiency and accuracy should be achieved since more controlled experiments will result in an increase of the overall computational resources. In any case, at least two controlled experiments are necessary to avoid the non-uniqueness problem previously described.

A. Optimisation space

The resulting antenna model is an improvement of the modelled antenna presented in [10] developed using a second order accuracy, in both space and time, FDTD algorithm as the forward solver [59]. The discretisation step is 1 mm and the time step is set according to the Courant stability criterion [15]. The geometry and the parameterisation of the antenna employed in this paper is very similar to the one presented in [10]. The dielectric properties of the antenna are assumed to be isotropic, linear, and dispersion-less and the source is modelled as a voltage source. **The received field is sampled in a simple free-space Yee cell with no additional conductivity or permittivity.** The only addition is an extra absorber, referred here as absorber-2 that surrounds the main absorber denoted as absorber-1 (Fig. 2). Full details of the GSSI 1.5 GHz antenna model are given in [10].

The optimisation space for the non-linear part of the FWI has ten dimensions:

- Absorber-1 Permittivity (ϵ_{a1})
- Absorber-1 Conductivity (σ_{a1})
- Absorber-2 Permittivity (ϵ_{a2})
- Absorber-2 Conductivity (σ_{a2})

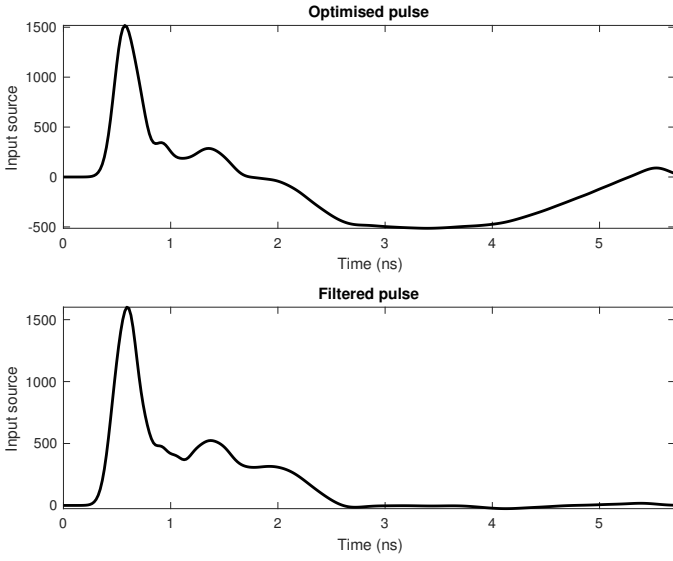


Fig. 6. The optimised pulse with and without post-processing. The low frequency component barely radiates through the antenna structure and corresponds to low frequency unfiltered static phenomena. To extend the pulse to more than 6 ns, the low frequency component is filtered out (filtered pulse) and subsequently zero-padding can be applied in a straightforward manner for the specified time-range.

- Source impedance (Z_t)
- HDPE permittivity (ϵ_h)
- HDPE conductivity (σ_h)
- PCB permittivity (ϵ_p)
- PCB conductivity (σ_p)

High-density polyethylene (HDPE) material forms the skid plate and the case of the antenna, while the printed circuit board (PCB) is glass fibre on which the metal bow-ties are printed [10]. The unknowns are primarily dielectric properties, thus the Jacobian can be mainly evaluated analytically. The derivative with respect to the impedance is derived numerically using a second order finite difference scheme (see equation (25)), due to lack of an analytic expression. Similarly, if the geometrical properties were part of the optimisation parameters (e.g. flare angle of bowties, dimensions of the absorber and so on), a numerical evaluation using a finite-difference scheme can be employed to evaluate the Jacobian.

B. Post-processing

The data collected for the controlled experiments are shown in Fig. 3. All of the manufacturer's standard post-processing filters, apart from stacking, that would normally be applied when using the 1.5 GHz antenna were disabled so that a raw response could be recorded. The only filter applied is shown in Fig. 3, and is a second order polynomial that describes low frequency current phenomena. The latter are filtered out through a simple subtraction.

C. Results

FWI is sensitive to the initial model and thus, a rational initial model should be chosen in order to ensure fast convergence

TABLE I. INITIAL AND OPTIMISED ANTENNA PARAMETERS

Parameters	Initial value	Optimised value
Absorber-1 ϵ	5	1.05
Absorber-2 ϵ	5	3.96
HDPE ϵ	2.5	1.99
PCB ϵ	1.5	1.37
Absorber-1 σ (S/m)	0.5	1.01
Absorber-2 σ (S/m)	0.5	0.31
HDPE σ (S/m)	0.01	0.013
PCB σ (S/m)	0.001	0.0002
Z_t (Ω)	75	195

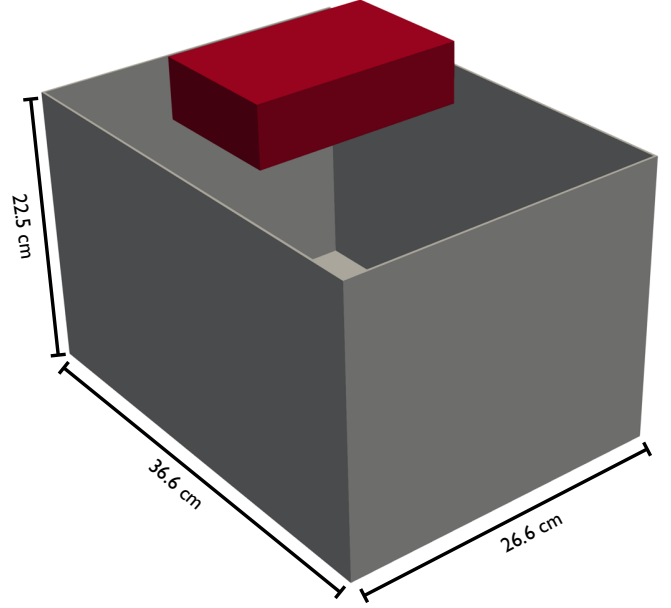


Fig. 7. A controlled experiment executed in order to validate the accuracy of the modelled antenna in a challenging scenario. The antenna (red) is placed on top of a hollow PEC box (grey).

and avoid local minimal. Here, the initial values were chosen based on realistic expectations of the dielectric properties of the absorbers, and the plastic elements of the antenna. For the excitation pulse, ideally a delta function should be used in order to excite the model with a wide frequency spectrum. However, when such an approach is used with the FDTD method, the result is a very noisy \mathbf{A} matrix which consequently creates the need for large λ , and furthermore increases η_λ . The excitation pulse should be chosen such as to incorporate a wide spectrum of frequencies in the model while minimising the numerical error – we used the pulse suggested in [10], which is a Gaussian pulse with 1.71 GHz central frequency.

Figure 4 shows $(\eta_\lambda, \rho_\lambda)$ and $(\eta_\lambda + \rho_\lambda, \lambda)$, generated by applying the hybrid FWI using different λ . It is evident that for $\lambda = 1$ the solution balances accuracy and stability. Using $\lambda = 0.01$ results in an unrealistic pulse and unrealistic dielectric properties (a relative permittivity of 45 for absorber-2) due to non-regulated noise both in the real and synthetic measurements. For values of $\lambda = 1, 5, 10, 20$ the resulting antenna models are very similar. **Notice that the hybrid**

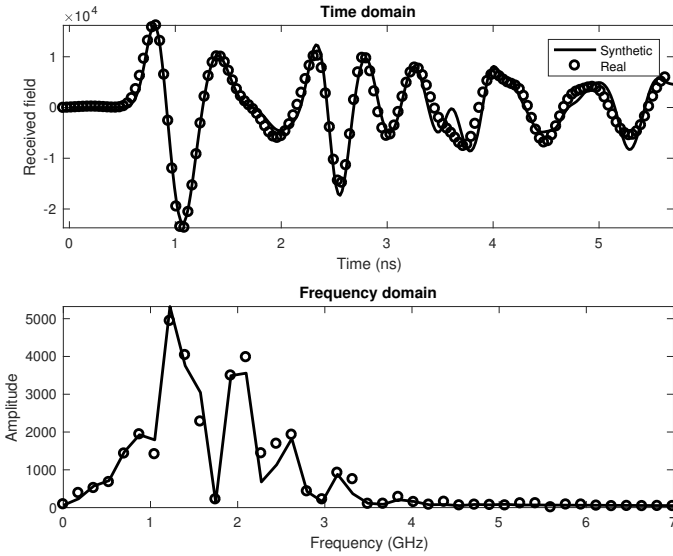


Fig. 8. Comparison between real and synthetic measurements of the experiments described in Fig. 7.

scheme should be executed for each λ . For the λ values used in the present study, the hybrid scheme converges smoothly in less than 10 iterations.

The synthetic and the real measurements for the controlled experiments are shown in Fig. 5. The modelled antenna can predict the near-field behaviour of the real antenna in a very challenging scenario, when the antenna is placed on top of a PEC.

Table I shows the initial model of the antenna and the resulting model of the hybrid linear/non-linear optimisation for $\lambda = 1$. The corresponding pulse for the parameters given in Table I is shown at Fig. 6. Due to the successful regularisation, the high frequency components associated with noise are repressed without compromising accuracy. Notice that the low frequency component of the pulse is barely radiated through the antenna structure primarily due to the small size of the bowties. Unfiltered low-frequency current phenomena are the reason that the hybrid FWI converged to the specific pulse. In order to apply the optimised pulse for a wider time range (> 6 ns), it is advised to filter out the low frequency component (see the filtered pulse in Fig. 6) in order to successfully zero-pad the pulse without creating sudden changes that will result in numerical errors. The measured fields using the filtered pulse have very small differences compared to the ones resulting from using the unfiltered pulse.

D. Validation

The modelled antenna is tested in two unknown scenarios which are not included in the hybrid optimisation process. The experimental setup of the first scenario is illustrated in Fig. 7. The antenna is placed on top of a hollow PEC box with dimensions $36.6 \times 26.6 \times 22.5$ cm. This setup was chosen in an effort to create a challenging scenario with respect to the directivity pattern. The antenna is surrounded

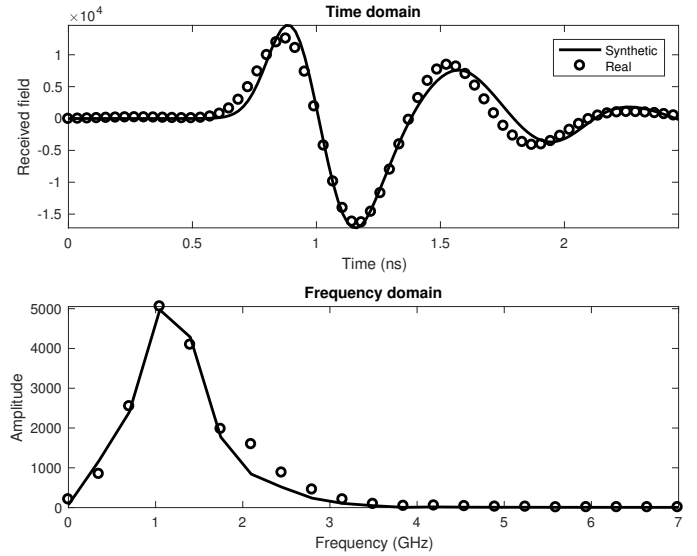


Fig. 9. Real and synthetic A-Scans when the antenna is coupled with dry sand.

by scattering sources, thus, an inaccurate directivity pattern will result in accumulative errors. In addition, the experiment is easily accessible and can be reproduced numerically in a straightforward manner. Fig. 7 shows the real and the synthetic measurements of the validation experiment. Both the early and the late reflections are in very good agreement indicating the validity of the modelled antenna.

The second scenario is the response of the antenna when coupled with very dry sand. The properties of the sand are chosen based on [60]. The relative permittivity is $\epsilon_r = 2.7$ and the conductivity is zero. The measurements took place in a sand box and the trace was cut at 3 ns to remove unwanted responses from the bottom of the sandbox and external sources of clutter. Fig. 9 shows the real data and the synthetic data generated using the optimised antenna model. The results are in good agreement showing that the antenna can successfully replicate near-field phenomena present in ground-coupled antennas.

IV. CONCLUSIONS

A hybrid linear/non-linear FWI scheme is presented which is used to simultaneously tune the dielectric properties and the excitation pulse of a modelled GPR antenna with a given known geometry, such as to minimise the misfit between synthetic and real measurements. The stability and the convergence of the suggested scheme is illustrated through modelling a GSSI 1.5 GHz commercial GPR antenna. The modelled antenna can successfully replicate the behaviour of the actual GSSI 1.5 GHz antenna even when the antenna is coupled with a PEC, where near-field phenomena are dominant. This approach is generally applicable for modelling commercial antennas where both the excitation pulse and its dielectric properties are usually unknown due to confidentiality issues, but the geometrical details can be obtained. Therefore there

is now the ability to more readily include accurate models of GPR antennas in simulations which, in turn, will provide improvements to model-based interpretations such as FWI and machine learning.

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